

In conclusion, we will present some of the dimensional quantities corresponding to plate motion with $Re^* = 3 \cdot 10^3$ in an electrolyte with $\sigma = 10^{12}$ 1/sec. Let $2a = 10^2$ cm. Then from Eq. (2.6) at $\delta = 0.4$ it follows that $\omega = 9 \cdot 10^4$ 1/sec, and from Eq. (4.4) and $v_0/u_0 = 0.39$ we have $v_0 = 1.2 \cdot 10^{-1}$ cm/sec; from Eq. (4.3), (2.5) we determine the amplitude of the maximum magnetic field intensity $H_0 = 2\pi I_0/\sec \approx 2.7$ G.

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UNSTEADY FLOW OF A NON-NEWTONIAN LIQUID WITH A POWER RHEOLOGICAL LAW PAST A FLAT PENETRABLE PLATE

V. I. Vishnyakov and A. P. Shakhorin

UDC 532.526.2,53

We analyze the problem of the unsteady flow of a non-Newtonian liquid with a power rheological law past a flat penetrable plate. In contrast with [1], where a similarly posed problem is treated for a pseudoplastic liquid, we solve the problem for a dilatant liquid.

For a non-Newtonian liquid with a power rheological law, the relation between the shear stress τ and the velocity gradient $\partial u/\partial z$ for plane motion has the form [2]

$$\tau = k \left| \frac{\partial u}{\partial z} \right|^{n-1} \frac{\partial u}{\partial z} \quad (n > 0),$$

where k and n are rheological constants of the medium; the case $n = 1$ corresponds to Newtonian liquid, $n < 1$ to a pseudoplastic liquid, and $n > 1$ to a dilatant liquid.

The problem of the flow of a non-Newtonian liquid with a power rheological law past an infinite flat plate in the presence of uniform suction of liquid depending on time according to a definite law was treated in [1]. This problem was solved for pseudoplastic ($n < 1$) and Newtonian ($n = 1$) liquids. We solve the problem in a similar formulation without restriction on the possible values of $n > 0$.

Moscow. Translated from Zhurnal Prikladnoi Mekhaniki i Tekhnicheskoi Fiziki, No. 1, pp. 91-94, January-February, 1980. Original article submitted January 19, 1979.

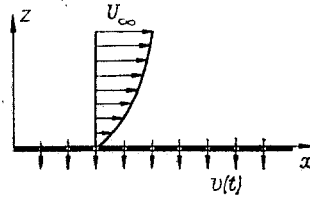


Fig. 1

We consider the unsteady flow of a power-law liquid past a flat surface $z = 0$ (Fig. 1) across which there is a transverse motion of liquid with the velocity

$$v(t) = \frac{\beta}{n+1} \left(\frac{U_\infty^{1-n}}{na} \right)^{-\frac{1}{n+1}} (t + t_0)^{-\frac{n}{n+1}}, \quad (1)$$

where $\beta = \text{const}$ is the velocity of the incoming flow; t , time; t_0 , initial time; and $a = k/\rho$.

In the boundary-layer theory approximation the equation of the nongradient motion of a power-law liquid can be written in the form

$$\frac{\partial u}{\partial t} + v(t) \frac{\partial u}{\partial z} = a \frac{\partial}{\partial z} \left(\frac{\partial u}{\partial z} \right)^n. \quad (2)$$

The problem of the existence and general character of the behavior of the solution of an equation of the type (2) is covered in detail in [3, 4].

An exact analytic solution of Eq. (2) for an arbitrary law of motion of the liquid $v(t)$ has not been obtained, but an exact self-similar solution of Eq. (1) exists.

The boundary conditions in the case under consideration are

$$u(0) = 0, u(\infty) = U_\infty. \quad (3)$$

The self-similar variable η and the velocity u are written in the form

$$\eta = \left(\frac{U_\infty^{1-n}}{na} \right)^{\frac{1}{n+1}} (t + t_0)^{-\frac{1}{n+1}} z, \quad u = U_\infty f(\eta). \quad (4)$$

By using (1) and (4) the solution of (2) and (3) can be reduced to the integration of the ordinary differential equation

$$\frac{n-1}{n+1} (\beta - \eta) = \frac{d}{d\eta} \left(\frac{df}{d\eta} \right)^{n-1} \quad (5)$$

with the boundary conditions

$$f(0) = 0, f(\infty) = 1. \quad (6)$$

Integrating (5) twice, we obtain

$$f(\eta) = \left[\frac{n-1}{2(n+1)} \right]^{\frac{1}{n-1}} \int_0^\eta (2\beta\eta - \eta^2 + \text{const})^{\frac{1}{n-1}} d\eta. \quad (7)$$

The solution of Eq. (5) is essentially different for $n < 1$ and $n > 1$, and therefore we treat these cases separately.

For $n < 1$ it is convenient to rewrite Eq. (7) in the form

$$f(\eta) = \left[\frac{1-n}{2(1+n)} \right]^{\frac{1}{n-1}} \int_0^\eta [(\eta - \beta)^2 + A^2]^{\frac{1}{n-1}} d\eta,$$

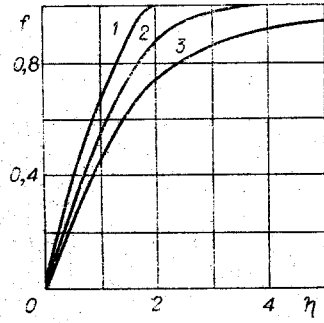


Fig. 2

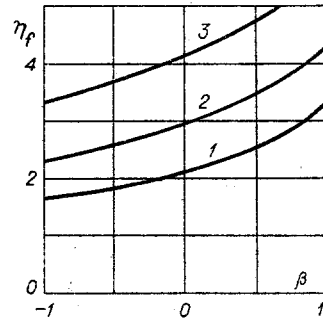


Fig. 3

where A is a constant to be determined.

By introducing the new variables $\xi = \eta - \beta$, and using boundary condition (6), we obtain

$$\int_{-\beta}^{\infty} (\xi^2 + A^2)^{\frac{1}{n-1}} d\xi = \left[\frac{2(1+n)}{1-n} \right]^{\frac{1}{n-1}}. \quad (8)$$

Evaluating the integral on the left-hand side of (8), we obtain a transcendental equation for the constant A

$$\begin{aligned} \frac{1}{2} A^{\frac{n+1}{n-1}} B \left[\frac{1}{2}, \frac{n+1}{2(1-n)} \right] + \frac{1}{2} A^{\frac{2}{n-1}} \beta B \left(1, \frac{1}{2} \right) F \left(-\frac{1}{n-1}, \frac{1}{2}, \frac{3}{2}, -\frac{\beta^2}{A^2} \right) \\ = \left[\frac{2(1+n)}{1-n} \right]^{\frac{1}{n-1}}, \end{aligned}$$

where B (p, q) is the beta function and F (α, β, γ, z) is the hypergeometric function.

For $n > 1$ we have

$$f(\eta) = \left[\frac{(n-1)}{2(n+1)} \right]^{\frac{1}{n-1}} \int_0^{\eta} [C^2 - (\eta - \beta)^2]^{\frac{1}{n-1}} d\eta, \quad (9)$$

where C is a constant to be determined.

Study of (9) shows that a limiting value $\eta = \eta_f$ exists such that for all $\eta > \eta_f$ $f(\eta) = 1$, i.e., shear perturbations for $n > 1$ are localized within a finite distance from the surface of the plate.

By introducing the new variable

$$(y - \beta)^2 = C^2,$$

we obtain two supplementary conditions:

$$f(\eta) = 1, \quad df/d\eta|_{\eta=y} = 0. \quad (10)$$

Taking account of (10), we have

$$\int_0^y [(y - \beta)^2 - (\eta - \beta)^2]^{\frac{1}{n-1}} d\eta = \left[\frac{2(n+1)}{n-1} \right]^{\frac{1}{n-1}} \quad (11)$$

Introducing the variables $\theta = \eta - \beta$ and $v = z - \beta$, and evaluating the integral in (11), we find an equation for C

$$y^{\frac{n+1}{n-1}} \left[\frac{1}{2} B\left(\frac{1}{2}, \frac{n}{n+1}\right) + 2^{\frac{n+1}{n-1}} \left\{ B_{\frac{y+\beta}{y}}\left(\frac{n}{n-1}, \frac{n}{n-1}\right) - B_{\frac{1}{2}}\left(\frac{n}{n-1}, \frac{n}{n-1}\right) \right\} \right] = \left[\frac{2(n+1)}{n-1} \right]^{\frac{1}{n-1}},$$

where $B_p(p, q)$ is the incomplete beta function.

Results calculated with the equations derived are shown in Figs. 2 and 3. Figure 2 shows dimensionless velocity profiles for various values of n and the injection parameter (suction) β [1) $n = 2$; 2) 1.25; 3) 0.5]. Figure 3 shows the position of the front of the shear perturbations as a function of the injection parameter (suction) β for various values of the rheological constant n [1) $n = 2$; 2) 1.25; 3) 1.15].

The authors thank K. B. Pavlov for a discussion of the results reported in the article.

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VISCOUS EXPLOSION DURING THE NONISOTHERMAL MOTION OF AN INCOMPRESSIBLE LIQUID

N. B. Aleksapol'skii and V. I. Naidenov

UDC 532.135

The hydrodynamic thermal explosion of an incompressible liquid moving under pressure in pipes was predicted theoretically in [1-3].

We present the hydraulic theory of a viscous explosion, which is caused by the non-linear temperature dependence of viscosity.

Let us consider the laminar motion of an incompressible liquid in a circular pipe of radius R and length L . The pressure is p_1 at the pipe inlet and p_2 at the outlet. The temperature of the liquid at the inlet cross section is T_0 , and a steady heat flux $\lambda \partial T / \partial r = q_w < 0$ is specified at the pipe walls (heat is removed from the liquid). The physical quantities λ , ρ , and C_p are assumed constant in the temperature range considered.

It is assumed that the Peclet number $Pe = uR\rho C_p / \lambda \gg 1$, so that axial heat conduction can be neglected in the heat-balance equation. We linearize the convective terms of this equation in the following way [4]:

$$v \text{ grad } T \approx \frac{Q}{\pi R^2} \frac{\partial T}{\partial x}, \quad Q = -\pi \int_0^R \frac{du}{dr} r^2 dr.$$

Thus, we consider the equation

$$\frac{\lambda}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) = \frac{\rho C_p Q}{\pi R^2} \frac{\partial T}{\partial x}.$$

Moscow. Translated from Zhurnal Prikladnoi Mekhaniki i Tekhnicheskoi Fiziki, No. 1, pp. 94-97, January-February, 1980. Original article submitted September 13, 1978.